PROCESSING OF OPERATING DEFLECTION SHAPES

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The article deals with measurement and visualization of the operating deflection shapes (ODS) on laboratory task. The aim is to measure Frequency Response Function (FRF) of selected points of the template. Together with visualization of their magnitude, real part, imaginary part or phase and show template’s ODS. The measuring chain consists of an accelerometer, laser and shaker. Data acquisition is performed via PULSE LabShop application. Visualization of processed data is accomplished in Matlab GUI application called “ODS app”. The article also contains the theoretical basis of the measurement principle along with setup of PULSE LabShop project and general description of Matlab GUI application components.

KEYWORDS
Auto-spectrum, cross-spectrum, deflection shapes, frequency transfer function, Matlab, transfer function

1 INTRODUCTION

Operating deflection shapes (ODS) analysis is a method for visualization the object dynamic under self-exciting forces. This method enables to identify, where the machine is moving with the maximum displacement, velocity or acceleration and which frequencies of excitation cause these problems. It is useful tool for the diagnostics of faults and for the development of new components or whole machines.

Method is based on experimental measuring of frequency response functions and interpreting them as an animation of a simplified geometric model representing the examined sample. The principle of this method is divided into two phases. The first phase represents measuring of FRF, i.e. determination of vibration magnitudes at single characteristic points and mutual phases (usually to one reference signal). The next step is the creation of an animation, which illustrates the shape of vibration during the excitation by selected frequency or by the combination of more frequencies. The movement of structure is usually amplified and slowed-down in the visualisation to make it suitable for visual inspection.

We can rank the most important pros: simplicity, great information value and wide range of implementations. The method allows e.g. identification of dynamic properties (resonance frequencies, identification of largest displacement location on part and design of flexible fitting, misery or unbalance).

This method grew up on its importance at the end of 80’s due to the increasing computing power and the implementation of two-channel (and later multi-channel) signal analysers into the diagnostics.

The operating deflection shapes analysis has become unnecessary part of machine diagnostics knowledge and this paper presents a laboratory task which is used for the education of mechanical engineers. The next chapter deals with a measurement of frequency response functions. It continues with the part which presents the relationship between frequency response functions and shapes, then an Matlab application for shape visualisation is introduced and finally, some results of the experiment are presented.

2 FREQUENCY RESPONSE FUNCTION

Frequency response function (FRF) represents the relation of the output and the input signal in a frequency domain. FRFs between measured points pairs are necessary for the ODS visualization [Herfert 2015], [Yonghui 2017], [Ganeriwala 2008]. It is accomplished in several steps. Two discretized signals are measured at the beginning. Let’s call the output channel of the system simply as a “signal” and the input as a “reference signal”. The signal is marked as y(kT) and the reference signal as x(kT). Both signals are then divided into data blocks with 2/3 overlay and M realizations of signals y(kT) ... y_M(kT), x_i(kT) ... x_W(kT) are extracted. All the realizations have N number of samples. In the next step, each of the blocks are weighted by Hanning window and obtained results are transformed using the Fast Fourier transform (FFT) into the frequency domain representations Y_i(f) ... Y_M(f), X_i*(f) ... X_W*(f). Complex conjugates are calculated by changing the sign of the imaginary part of complex numbers and these representations are marked with superscript “*”:

\[ Y_i(f) \ldots Y_M(f), X_i*(f) \ldots X_W*(f) \] 

Now, it is possible to calculate auto-spectrum \( S_y \) of the signal, auto-spectrum \( S_x \) of a reference signal. And a cross spectrum \( S_{xy} \).

Figure 1. Dividing the measured signal into M blocks and weighting by Hanning window

The auto-spectrum (also known as power spectrum) of the signal weighted block is computed as a product of signal’s Fast Fourier transform and corresponding complex conjugate. The resulting auto-spectrum is computed as an average over M measurement realizations.

\[ S_y(f) = \frac{1}{M} \sum_{i=1}^{M} Y_i(f) \cdot Y_i^*(f) \]  \hspace{1cm} (1)

The averaging smooths the resulting spectrum but also consumes measurement time, because more samples are needed.

The auto-spectrum of the reference signal is calculated in the same way:

\[ S_x(f) = \frac{1}{M} \sum_{i=1}^{M} X_i(f) \cdot X_i^*(f) \]  \hspace{1cm} (2)
The cross-spectrum is computed as a multiplication between
the Fourier transform of the reference signal and the

corresponding complex conjugate of signal’s Fourier transform:

\[ S_{xy}(f) = \frac{1}{M} \sum_{i=1}^{M} X_i(f) \cdot Y_i^*(f) \]  

(3)

It is also possible to calculate the "backwards" cross-spectrum:

\[ S_{yx}(f) = \frac{1}{M} \sum_{i=1}^{M} Y_i(f) \cdot X_i^*(f) \]  

(4)

Frequency response function is simply the cross-spectrum divided
by the auto-spectrum of the reference signal:

\[ H(f) = \frac{S_{xy}(f)}{S_{yy}(f)} \]  

(5)

Alternatively, it is possible to calculate the FRF as the signal
auto-spectrum divided by the cross-spectrum:

\[ H(f) = \frac{S_{xy}(f)}{S_{xx}(f)} \]  

(6)

If the frequency response function is calculated as H1
approach, the processing can suppress the noise of output
signal y and if the function is calculated in a H2 way, the noise
in the input signal is suppressed. In the case, when it is supposed
that both signals are affected by the noise on a comparable
level, the "H3" is computed as a geometrical average of H1 and
H2.

\[ H(f) = \sqrt{H_1(f) \cdot H_2(f)} \]  

(7)

Because the signal from the laser is delayed by 1.28 ms, this
time must be added also to the accelerometer channel (good
synchronization is a key preposition of this kind of
measurement). The analyser also generates a white noise signal
for the structure’s excitation. This signal is sent to the amplifier
and the shaker’s coil is powered.

White noise is a commonly used measurement signal, which
has theoretically infinite frequency range. Practically it must be
reduced to some finite range, in the measurement presented in
this paper, the frequency span was 12.8 kHz. Another testing
signals can also be used to identify various systems. The
simplest one is sine testing signal, another are: swept sine,
impulse, step, spread spectrum signal [Vala 2016], [Proto
2016].

Frequency response functions were measured in the range of
6.4 kHz. Sampling frequency is 2.56 times greater, which is
16 384 samples per second. This satisfies the Nyquist–Shannon
sampling theorem with a suitable reserve. The power of two
number is eligible for Fast Fourier transform used later. The
chart consisted of 1600 bars, which means that the block were
4096 samples long (2.56 times more); it corresponds to 250 ms.
FRFs were computed as an average from 100 blocks.

In next figures, there are examples of spectra and FRF, which
were obtained during the measurement of point number 88.
Auto-spectra (Fig. 4) express which frequencies are present in
the signal. Several frequencies in laser signal are dominant; it
can be said, that these are the frequencies at which the sample
tends to vibrate. Auto-spectra are real numbers, while the
cross-spectrum is a sort of complex numbers and brings the
information of the phase (Fig. 5) FRF includes two information
because these functions are complex. Several approaches how
to graphically demonstrate this FRF exists, but probably most
often the magnitude and the phase both depending on the
frequency are depicted. In this case the magnitude part shows
how many times the output’s amplitude is greater than the
input’s amplitude at selected frequency. However, for the
purpose od ODS, the imaginary part (Fig. 7) is the most
important one and is used for the illustration of the shape.
FRFs are presented for the purpose of ODS visualization in this
paper, but these can be found in many more applications such
are modal analysis [Maia 1997], [Agneni 2004], [Agneni 2006]
or is a part in the design in popular passive and active vibration
control [Wrona 2016A], [Wrona 2016B], [Wrona 2016C].

Figure 2. Sample’s mesh with attached accelerometer and laser located
at the selected measurement point.

The first step is to draw a mesh on a studied object. In this
demonstration task, the number of 164 measured points is
defined on the sample, the positions of the points reflect the
sample’s geometry. Using 6 bolts, the sample was fastened to
the shaker and an accelerometer was glued onto the
appropriate point in the center of this attachment. This
accelerometer measures the reference signal and remains in
the same position during all of 164 frequency response
functions measurements. The output signal was measured
using the laser vibrometer. The both signals are processed in
the signal analyser BK 3560C and Pulse LabShop software.
Figure 4. Auto-spectra of measured signals

Figure 5. Cross-spectrum between measured signals

Figure 6. Frequency response function – magnitude and phase

Figure 7. Frequency response function – real and imaginary part
3 DEFLECTION SHAPES

In application presented in this paper, operating deflection shapes will be extracted from imaginary parts of measured response functions. The relationship between FRFs measured on a laboratory sample and final deflection shape is best to show on an example. Let’s say, we want to study the deflection shape of the sample during the frequency of 1212 Hz. We will focus on the measurement point number 88, whose FRF was captured and described in the previous chapter. The value of imaginary part at the frequency of 1212 Hz is approximately -12. This number is placed into a mesh grid as a third value in a 3D surface plot. While this process is repeated for all measured points, the final shape for 1212 Hz is acquired.

![Figure 8. The relationship between measured FRF and the operating deflection shape](image)

4 ODS APPLICATION

Graphical user interface was designed to visualize the measured data. This application enables to import measured FRFs saved as text files in ASCII format. These functions can be displayed as magnitude, phase, real and imaginary part. The selection of displayed functions is also implemented and is accessible through context menu. The main part of GUI is the visualization of the deflection shape according to the selected frequency. This shape can be animated, and the video can be saved in an avi file.

![Figure 9. ODS application GUI preview](image)

5 EXPERIMENTAL RESULTS

Results acquired on a laboratory plant are concluded in this chapter in a graphical form. Figures depict ODSs at a given frequency. These illustrations enable to understand which places on the laboratory samples have vibrationally risky behaviour and which frequencies are connected to these problems. For example, if we look at the Figure 12, which illustrates the shape at the frequency of 1220 Hz, there can be seen, that the left corner, right edge and the area on the right side have the highest relative amplitudes.

![Figure 10. Shape at 684 Hz](image)

![Figure 11. Shape at 952 Hz](image)

![Figure 12. Shape at 1220 Hz](image)

![Figure 13. Shape at 1704 Hz](image)
6 CONCLUSIONS

This paper presents a laboratory task designed for operating deflection shape processing. The mathematical procedure used for measuring frequency response functions was introduced together with a measurement chain for the diagnostics of these functions. Laboratory equipment included a vibration shaker with its signal amplifier, signal analyser and signal processing software, piezoelectric accelerometer and Doppler laser vibrometer. The relation between frequency response functions and operating deflection shape was explained. A special application designed for the visualization of measured shapes was also presented and finally the experimental results obtained on a laboratory sample are shown.

The main goal of this paper is to simply demonstrate the acquiring of operating deflection shapes in several simple steps: measurement FRFs on a laboratory sample, transferring imaginary parts onto a mesh and visualizing results.

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REFERENCES


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