

DEVELOPMENT OF MATHEMATICAL MODELS DESCRIBING THE PROCESS OF FRICTION AND WEAR OF META-ARAMID

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The study aims to describe the properties of heat-resistant coatings of tribological purpose based on meta-aramid and obtain mathematical models, that will provide simple usage of this data. These are results of experiments that show the dependencies of coefficient of friction and mass wear on two factors: load and filler content. All the experimental data is obtained for such filler materials: boron nitride, graphite, molybdenum disulfide. As a result, the number of mathematical equations that describe this experimental data is obtained. These equations allow to get interpolated value for any combination of arguments, present smooth 3D graphs, that show the form and character of all the dependencies.

KEYWORDS

Mathematical model, Coating, tribological, Meta-aramid, Approximation, Equation, Load, Filler, Coefficient of friction, Mass wear

1 INTRODUCTION

Modern machines and mechanisms have components that work under high loads. The most problematic issues here are the durability and reliability of friction pairs of heavily loaded machines. To solve the above-mentioned issues, new, modern materials of tribological purpose are used, polymer materials [Sezer Hicyilmaz 2021]. The issue of mathematical description of the properties of these materials for the purpose of their convenient analysis and usage is important nowadays.

One of the promising ways of usage the above-described materials is to apply them to the metal surfaces of parts, which allows, on the one hand, to use important characteristics of the main material of the part, such as strength, but to ensure excellent material properties in the friction zone, such as wear intensity, friction coefficient [Klymenko 2022, Klymenko 2014]. Aromatic polyamides [Buketov 2024, Sapronov 2017, Buketov 2016, Panda 2011], meta-aramid (Nomex), are a promising material for obtaining tribological coatings.

However, it should be noted that meta-aramid, like other aromatic polyamides, has low adhesion to metals, which makes

it difficult to obtain high-quality coatings [Valicek 2016, Jurko 2011, Panda 2013a & 2021, Jurko 2012]. The influence of most solid layered fillers on the conditions of formation and performance of such coatings is also unknown.

Polyimide-based coatings have good adhesion to various materials such as metals, polymers, carbon, silicon-based materials (glass fiber, carbon fiber), etc. Aromatic polyamides are usually coated in a two-step process: in the first step, a polyamide acid solution is applied to the substrate, and in the second step, thermal or chemical imidization occurs [Panda 2011 & 2014, Jurko 2013, Dyadyura 2017a, Nahorny 2022]. There are several coating methods such as solution deposition, immersion [Sukhodub 2018a, Zaloga 2019 & 2020], foaming [Acerbi 2020, Ren 2022, Ding 2022] or vapor deposition [Dyadyura 2017b, Kivimaa 2019, Sassanelli 2020, Panda 2020 & 2022], chemical deposition polymerization [Pandova 2018 & 2020], etc. New methods for applying polymer coatings have also been developed, such as liquid flame spraying, etc. [Harnicarova 2019, Sukhodub 2019].

There is a technique [Klymenko 2014] of obtaining antifriction coatings based on the aromatic polyamide Phenylon, which is a copolymer of meta-aramid. But it should be noted that this copolymer is not synthesized in Ukraine and European countries, and its production has never reached industrial scale.

The purpose of this work is to study and describe the properties of heat-resistant coatings of tribological purposes based on meta-aramid and obtain mathematical models. Since the dependencies between the composition of the material and its properties can be complex, the task is to propose and implement a method of mathematical description of the obtained experimental dependencies.

2 MATERIALS AND METHODS

Polymer coatings of thickness 80...100 μm were obtained by the method described in [Klymenko, 2022], namely by applying a solution of meta-aramid with a suitable filler to the surface of a metal substrate with subsequent evaporation of the solvent by drying. Fillers of these materials were layered solid lubricants: graphite, boron nitride, copper phthalocyanine and molybdenum disulfide. Selected antifriction fillers were used in finely dispersed form with a particle size of 1–2 μm . The filler content varied from 0 to 20 mas.%.

As a starting material for obtaining coatings, a finely dispersed powder with a bulk density of 0, 25 - 0,32 g/cm³ was used.

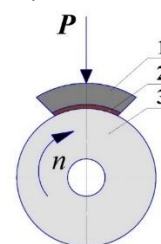


Figure 1. Scheme of the friction: P – load; n – frequency of rotation of the counter body; 1 – metal substrate; 2 – polymer coating; 3 – counter body

Dimethylacetamide (DMAA), which is widely used for dissolving aromatic polyamides, was used as a solvent. The samples were dried in a drying oven at a temperature of 150...165°C for 45...55 minutes. The study of the tribological properties of composite coatings based on meta-aramid was carried out in lubrication friction mode at a load of $P = 2,5 \dots 10 \text{ MPa}$ and a sliding speed of $v = 1 \text{ m/s}$ on a friction machine SMT-1 according to the disc-pad scheme (Fig. 1), on a counterbody made of Steel 45 with a hardness of 45–50 HRC and a diameter of 50 mm.

As a rule, a mathematical model is understood [Klymenko, 2022] as an approximate description of the basic patterns of a class of objects, systems, or processes using mathematical symbols in the form of equations, inequalities, etc. The development of mathematical models of technological processes is primarily aimed at conducting a computational experiment procedure.

A review [Sukhodub 2018b, Panda 2013b] of literary sources allows us to highlight the following main properties of mathematical models: completeness, accuracy, adequacy, economy, robustness, productivity, and visibility. Polynomial two-factor interpolation and approximation methods were used to solve the problem of describing experimental data. The generalized form of the approximating polynomial is presented in (1).

$$f(x, y) = \sum_{\substack{n=0..k \\ m=0..p \\ i=0..q}} a_i \cdot x^m y^n \quad (1)$$

In the above expression, i is determined by the number of terms of the polynomial, m and n are determined by the degree of the polynomial. Under somewhat values of i , the polynomial can be complete, then the maximum values of m and n are the same. Calculations were performed using Mathcad 14 software.

3 RESULTS

At the first stages of research, experimental data was obtained on the dependence of the coefficient of friction f and mass wear I on the load, filler content for different fillers cases. Dependencies for mass wear are presented in Figure 2.

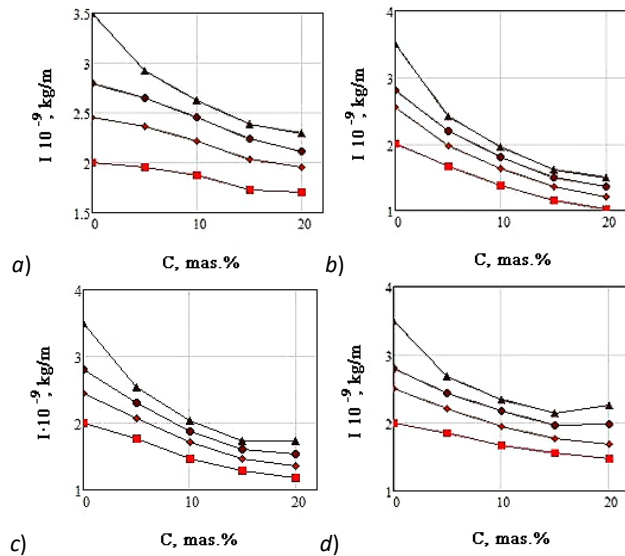


Figure 2. Experimental dependences of mass wear on the concentration of the filler with different natures of the filler: a) boron nitride, b) copper phthalocyanine, c) graphite, d) molybdenum disulfide

Similar experimental dependences are obtained for the friction coefficient; they are presented in Figure 3.

The forms of above dependencies have simple general trends, but their exact behavior is complicated. The issue of a mathematical description of the experimental results obtained is important. We will describe the above data as the dependences $f(C, P)$ and $I(C, P)$, that is, the dependences of functions on two arguments. Compared to approximation by functions of one argument, this will significantly reduce the number of equations that describe the system, as well as allow finding the values of these functions at any intermediate points of the studied range, but it will also lead to an increase in the size of the interpolation function. Since the above experimental data

is already the result of averaging raw experiment results, we will use interpolation to describe the data.

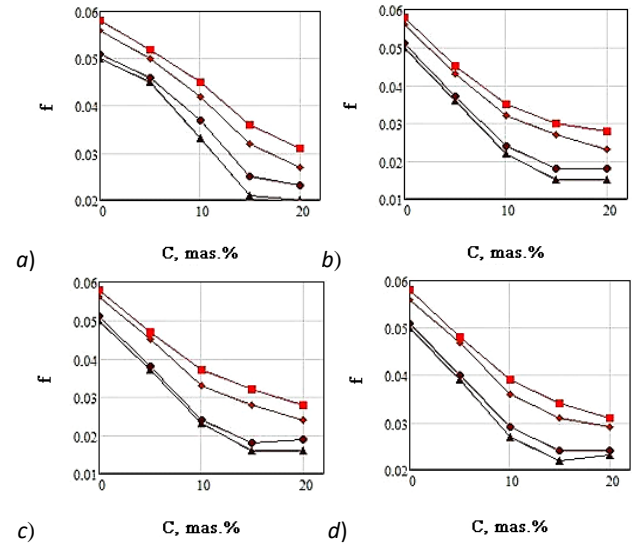


Figure 3. Experimental dependences of the coefficient of friction on the concentration of the filler with different natures of the filler: a) boron nitride, b) copper phthalocyanine, c) graphite, d) – molybdenum disulfide

Given the lack of data on the type of dependence that could describe the experimental data, we will use a polynomial for data interpolation, the number of members of it will be equal to the number of experimental points on one graph (20 members) (2). The application limits of this formula.

$$\begin{aligned} f(C, P) = & a_0 + a_1 P + a_2 P^2 + a_3 P^3 + a_4 P^4 + a_5 C + a_6 C P + \\ & + a_7 C P^2 + a_8 C P^3 + a_9 C P^4 + a_{10} C^2 + a_{11} C^2 P + a_{12} C^2 P^2 + \\ & + a_{13} C^2 P^3 + a_{14} C^2 P^4 + a_{15} C^3 \\ & + a_{16} C^3 P + a_{17} C^3 P^2 + a_{18} C^3 P^3 + a_{19} C^3 P^4 \\ & C = 0 \dots 20 \text{ mas. \%} \\ & P = 2.5 \dots 10 \text{ MPa} \end{aligned} \quad (2)$$

where f is coefficient of friction, C is filler content, mas. %, P is load, MPa, $a_0 \dots a_{19}$ are polynomial coefficients.

Table 1. Values of empirical coefficients for $f(C, P)$

Coeff icient	The value of the coefficients of the polynomial			
	Boron nitride	Copper phthalocya nine	Graphite	Molybdenu m disulfide
a_1	0.05	0.05	0.05	0.05
a_2	-0.0024667	-0.0043833	-0.0053667	-0.0081833
a_3	0.00067	0.00037167	0.0005866	0.001235
a_4	-0.0000693	-0.0000327	-0.0000453	-0.0000807
a_5	0.000002	0.00000113	0.0000013	0.0000018
a_6	0.0061333	0.0061333	0.0061333	0.0061333
a_7	0.0006477	0.0010978	0.0023089	0.0041378
a_8	-0.0003743	-0.000244	-0.0004673	-0.0008557
a_9	0.0000378	0.00002568	0.0000399	0.0000592
a_{10}	-0.0000010	-8.5333e-7	-0.0000011	-0.0000013
a_{11}	-0.00136	-0.00136	-0.00136	-0.00136
a_{12}	-0.0001293	-0.0001693	-0.0003706	-0.0006987
a_{13}	0.0000745	0.00003347	0.0000675	0.0001416
a_{14}	-0.0000076	-0.0000038	-0.000006	-0.0000098
a_{15}	2.1867e-7	1.3333e-7	1.8133e-7	2.24e-7
a_{16}	0.0000747	0.00007467	0.0000747	0.0000747
a_{17}	0.0000089	0.00000836	0.0000178	0.0000356
a_{18}	0	0	0	0
a_{19}	4.5511e-7	1.7778e-7	2.7022e-7	4.9778e-7
a_{20}	-1.28e-8	-6.4e-9	-8.5333e-9	-1.1378e-8

To describe the dependence for a specific material, it is necessary to substitute the values for the empirical coefficients $a_0 \dots a_{19}$ in the polynomial, obtained by interpolation. The

values of coefficients for coefficient of friction dependency are given in Table 1.

To visualize the obtained dependencies, we will construct spatial graphs combining the experimentally obtained points and the interpolation surface. Each graph represents a separate material with the $f(C, P)$ dependence for it (Figure 4).

Similarly, the dependences of mass wear on the same parameters $I(C, P)$ can be obtained. The general form of the polynomial (2) remains unchanged, and only the function (and the value of the coefficients) changes.

$$I(C, P) = a_0 + a_1 P + \dots + a_{19} C^3 P^4 \quad (5)$$

Coefficients $a_0 \dots a_{19}$ remain unchanged by position but obtain new values.

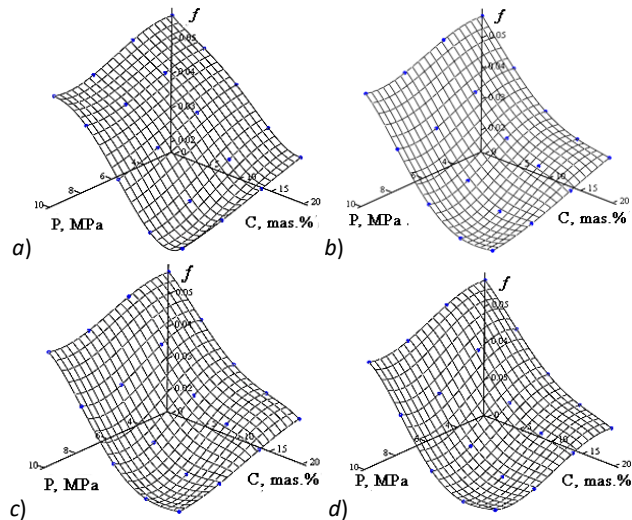


Figure 4. Graphs of dependencies $f(C, P)$ for materials: a) boron nitride, b) copper phthalocyanine, c) graphite, d) molybdenum disulfide

This is due to the organization of experimental studies so that the conditions of their conduction are the same when measuring the coefficient of friction and mass wear. The values of coefficients $a_0 \dots a_{19}$ for dependence (5) are given in Table 2.

Table 2. Values of empirical coefficients for $f(C, P)$

Coefficient	The value of the coefficients of the polynomial			
	Boron nitride	Copper phthalocyanine	Graphite	Molybdenum disulfide
a_1	1.0	0.4	1.0	0.7
a_2	0.16367	0.4215	0.1485	0.217
a_3	-0.025333	-0.06945	-0.02865	-0.030167
a_4	0.001573	0.00418	0.00182	0.00188
a_5	-0.000035	-0.000086	-0.000038	-0.0000413
a_6	0.57	0.95	0.57	0.76
a_7	-0.12363	-0.31408	-0.1136	-0.15608
a_8	0.01951	0.045046	0.014409	0.017437
a_9	-0.00134	-0.0026742	-0.000832	-0.0009969
a_{10}	0.000032	0.00005524	0.0000167	0.0000209
a_{11}	-0.08	-0.144	-0.08	-0.112
a_{12}	0.025693	0.054893	0.021787	0.028893
a_{13}	-0.004078	-0.0079213	-0.0029413	-0.0032413
a_{14}	0.000275	0.00046667	0.0001685	0.0001755
a_{15}	-0.000006	-0.00000955	-0.0000033	-0.0000037
a_{16}	0.0048	0.008	0.0048	0.0064
a_{17}	-0.001675	-0.0031076	-0.001472	-0.0018062
a_{18}	0.000255	0.00044338	0.000204	0.0002059
a_{19}	-0.000016	-0.00002588	-0.000012	-0.0000109
a_{20}	3.84e-7	5.2622e-7	2.2756e-7	2.1333e-7

For this set of data, it is also possible to build graphic dependencies that highlight the features of the behavior of the function for different materials (Figure 5).

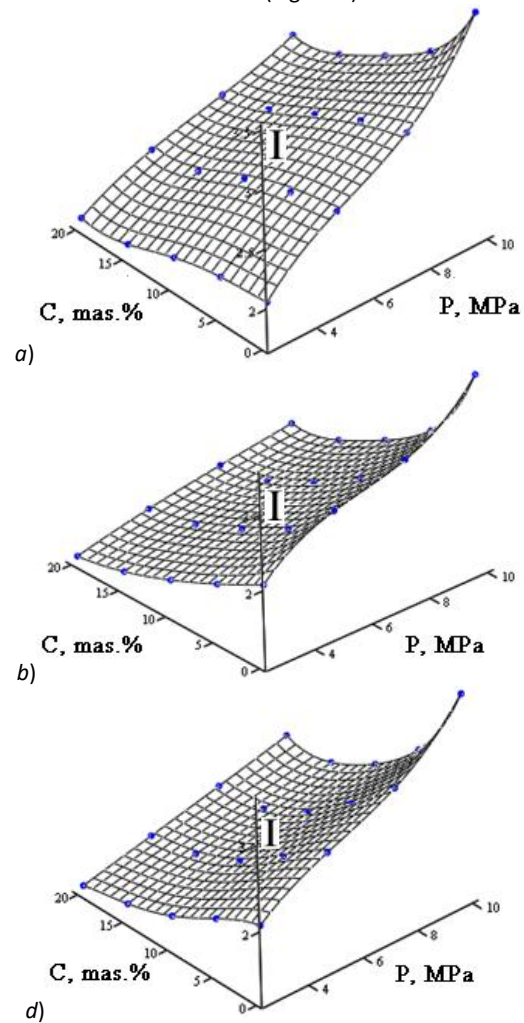


Figure 5. Graphs of dependencies $I(C, P)$ for materials: a) boron nitride, b) copper phthalocyanine, d) molybdenum disulfide

Figure 5 shows that the obtained dependencies describe the experimental data well and provide important information about the behavior of the functions in the studied range of values.

4 CONCLUSIONS

The usage of materials with high tribological properties such as coatings for machines that work under heavy loads is the way to increase durability, reliability etc. And the best results may be obtained if we use the materials with the best set of properties for every case. The experimental dependencies between material (meta-aramid) composition and set of properties were already obtained.

As a result of the performed data approximation, the results of experiments became more systematic, a few empirical dependencies were obtained by interpolating the experimental data surfaces and now can be presented on 3D graphs for a more visual perception. Obtained models allow us to calculate the properties of given material from its composition, also we can get the needed materials compositions for given set of properties. All these results can help to find the proper material compositions and provide the best properties of high loaded machine parts.

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